

Eight Legs Rimless Wheel Robot Model Driven on Level Ground Using one actuator

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Abstract

It is outstanding that a rimless wheel (RW) needs actuators to walk on the level ground. There is the primary test hard to discover an appropriate control framework to accomplish a stable RW movement. There is the model of the eight-legged under actuated rimless wheel with the middle. To start with, we created 4-DOF numerical model of an under actuated rimless wheel (URW) and figured the condition of movement as per the Lagrange's technique. We likewise perform numerical recreations utilizing the model created and demonstrate that a steady stride can be produced with the appropriate introductory condition and physical parameters. The numerical recreations demonstrate that, by embracing this control framework, the URW with middle can walk steadily on level ground, and the URW can be driven with an extensive variety of speed and high productivity by changing the control parameter.

Keywords

Robot,
level ground,
wheel,
eight legs

1. Introduction

In the late 1980s and mid-1990s, McGeer spearheaded uninvolved dynamic strolling by presenting the rimless wheel [1]. The progression of the rimless wheel was considered fundamentally. Since the presentation of the rimless wheel, its latent steadiness on a delicate slope was resolved to be 1-period half steady[5]. With frictional misfortunes, the framework is asymptotically steady. In this movement, the vitality lost when the swing foot hits the ground is recuperated by gravitational potential vitality. In this way, a completely inactive dynamic walker can just stroll down an incline. To acknowledge level-ground strolling, dynamic power, supplanting gravity, must be infused into the biped robot. McGeer proposed different techniques including, 1) applying an indiscreet push as the positioning leg leaves the ground, 2) changing the leg length, and 3) using response torque against an inclining middle. In 2009, F. Asano and Zhi-Wei Luo explore on "Asymptotically stable biped step which can produce in light of security standard of a rimless wheel" [2, 3]. That examination was contrasted and those for the rimless haggles significant steadiness standard determined. Albeit numerous investigations have gotten the main control technique for level-ground strolling, there are generally few papers on the fourth control strategy. From a tasteful point of view, it is normal for a biped robot to have a middle. Also, from a building viewpoint, numerous instruments can be included in the middle, in this way incredibly growing the application extent of a biped robot. Thusly, it is essential to incorporate and control the middle of a biped robot. The rimless wheel (RW) which was one of the least difficult utmost limit cycle walkers [4], built up a consistent single – step cycle when strolling on a slant latently. In this manner, the ideal strolling states were found and created in detached utmost passive limit cycle walker. Underactuated Rimless Wheel Robot Model

Fig-1 demonstrates the model of a URW with a middle. This walker comprises of an eight-legged rimless hagle middle connection. The range of the RW which is proportional to the leg-outline length is l (m) and the middle length is L_t (m). The relative blessed messenger between two contiguous edges, (rad). The mass of the RW is m_1 (kg), and that of the middle is m_2 (kg).The add up to mass is $m = m_1 + m_2$ (kg).the middle connection is associated with the RW at the inside position, and the snapshot of idleness about the joint is I_1 ($\text{kg}\cdot\text{m}^2$) for RW and I_2 ($\text{kg}\cdot\text{m}^2$) for the middle.

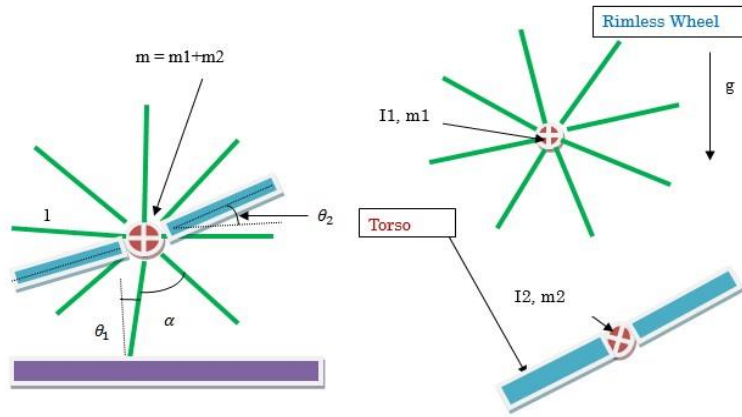


Fig. 1: An Underactuated rimless wheel robot model

The URW can apply a joint torque between the torso and RW. We assume that the contact purpose of the positioning leg with the ground does not slide or bounce amid movement. The URW display at that point turns into a 4-DOF framework. We characterize as the precise position of the RW with the regard to vertical, and as the rakish position of the middle connection as for level, individually.

2. Equation of Motion

Let $q = [x \ z \ \theta_1 \ \theta_2]^T$ be the generalized coordinate vector.

Kinetic Energy of the walking robot,

$$K = \frac{1}{2} m (\dot{x}_1^2 + \dot{z}_1^2) + \frac{1}{2} (I_1 \dot{\theta}_1^2 + I_2 \dot{\theta}_2^2) \quad (1)$$

Potential Energy of the walking robot,

$$P = mg(Z + L \cos \theta_1) \quad (2)$$

The walking robot equation of motion then becomes

$$M(q)\ddot{q} + h(q, \dot{q}) = Su + J^T \lambda \quad (3)$$

$$M(q) = \begin{bmatrix} m_1 + m_2 & 0 & L(m_1 + m_2)\cos[\theta_1] & 0 \\ 0 & m_1 + m_2 & -L(m_1 + m_2)\sin[\theta_1] & 0 \\ L(m_1 + m_2)\cos[\theta_1] & -L(m_1 + m_2)\sin[\theta_1] & I_1 + L^2(m_1 + m_2) & 0 \\ 0 & 0 & 0 & I_2 \end{bmatrix}$$

$$h(q, \dot{q}) = \begin{bmatrix} -d\theta_1^2 L(m_1 + m_2)\sin[\theta_1] \\ (m_1 + m_2)(g - d\theta_1^2 L\cos[\theta_1]) \\ -2gL(m_1 + m_2)\sin[\theta_1] \\ 0 \end{bmatrix}$$

3. Collision Equation

The inelastic crash of the foreleg (the following position leg) with the ground is then demonstrated as

$$M(q)^{\cdot} q^{+} = M(q)^{\cdot} q^{-} + J_1^T \lambda_1 \quad (4)$$

Where the superscripts "-" and "+" remain instantly previously and quickly after effect. Note that q in Eq. (4) is equivalent to $q^{-} = q^{+}$. The drive vector given as the zero time necessary for the rash power at effect.

4. Control Method

To hold the middle which is running one engine. On the off chance that we are setting up an immaculate control framework then middle can get high proficient vitality. The control yield is expected to accomplish steadier stride from URW.

$$s = \begin{bmatrix} 0 \\ 0 \\ 1 \\ -1 \end{bmatrix}, \text{ where } s \text{ is control input of motor.}$$

$$u = -50 * \theta_1 + 0.03; \quad (5)$$

$$\text{Lambda} = \text{inv}(J * \text{inv}(M) * J') * (J * \text{inv}(M) * (h - s * u)); \quad (6)$$

$$N = J * \text{Lambda} + s * u;$$

This walker can apply a joint torque, u (Nm), between the positioning leg and the middle. The middle capacities as a response wheel for the RW; the positioning leg can utilize the response torque for the drive. Lambda is the Lagrange undetermined multiplier that speaks to the vertical ground response drive.

5. Gait Generation and Numerical Simulation

Utilizing a changed rendition of ODE45 in Matlab R2015a. We consider here some record made in Matlab, for example, fundamental, impact, parameter and so forth. Crash setup meets with machine exactness. We utilize is the edge of rimless wheel separately. α is the point between the rimless wheel leg. m2 are mass of RW and middle individually. L is the leg length of the rimless wheel is the length of the middle. g is the increasing speed because of gravity.

Table 1: Physical Parameter settings

m1	1 kg	I_1	1 kg. m ²
m2	1 kg	I_2	1 kg. m ²
L	1 m	G	9.81 m/S ²
Lt	1 m	α	$\pi/4$ rad

The Fig-2 shows the simulation movie of URW robot with Torso driven on level ground (Simulation Movie). This eight legs robot can walk continuously on the level ground without fall down.

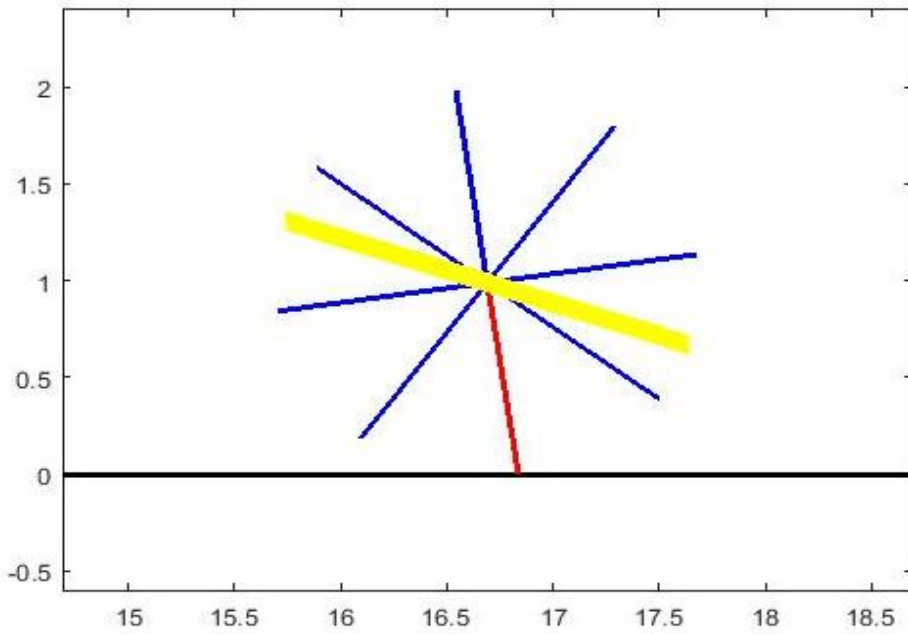


Fig. 2: URW robot with Torso driven on level ground (Simulation Movie) Fig - 3 to Fig - 9 demonstrate the reenactment after effects of URW with middle on the level ground. Here we utilize the $T_{set} = 20$ sec the development of the progression time frame for the initial 100 stages in the strolling walk produced in all figures. We can see that the URW 4-DOF eight-legged robot displays period 4-movement and get a steady step.

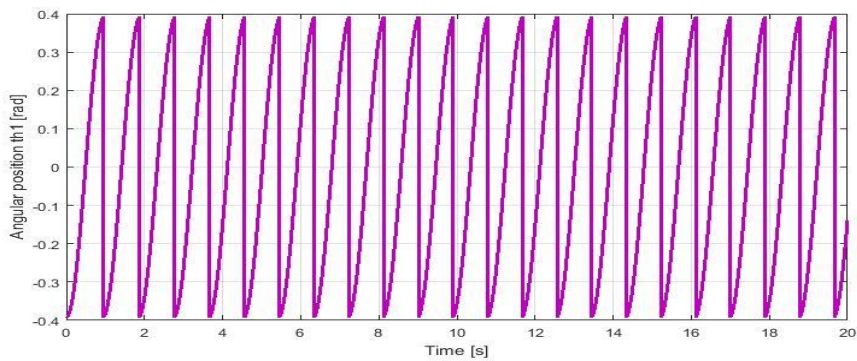


Fig 3: Angular position of th1 with time

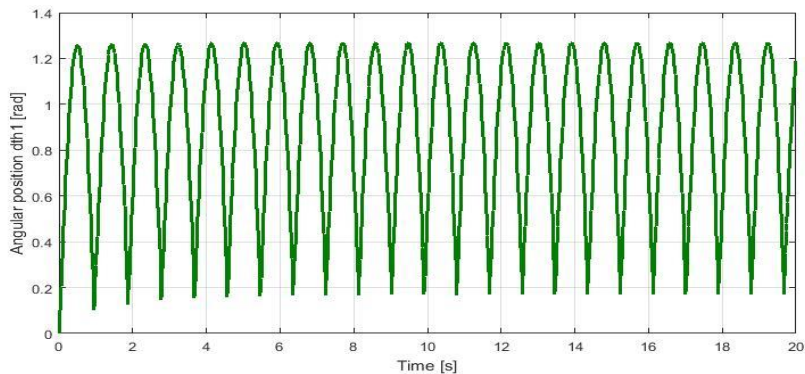


Fig. 4: Angular velocity of dth1 with time

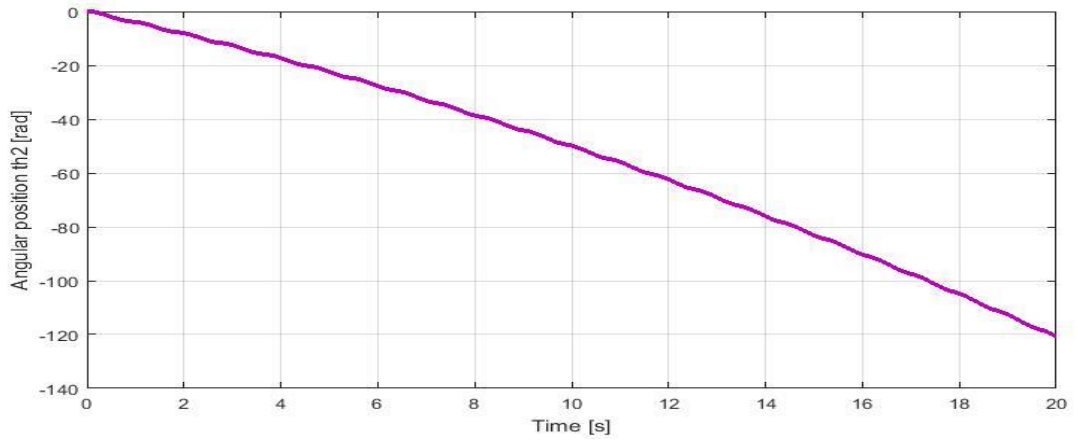


Fig. 5: Angular position of θ_2 with time

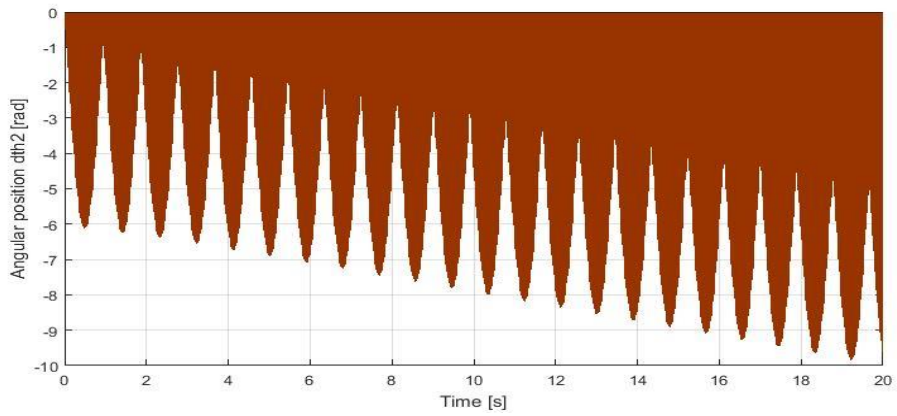


Fig. 6: Angular position of $d\theta_2$ with time

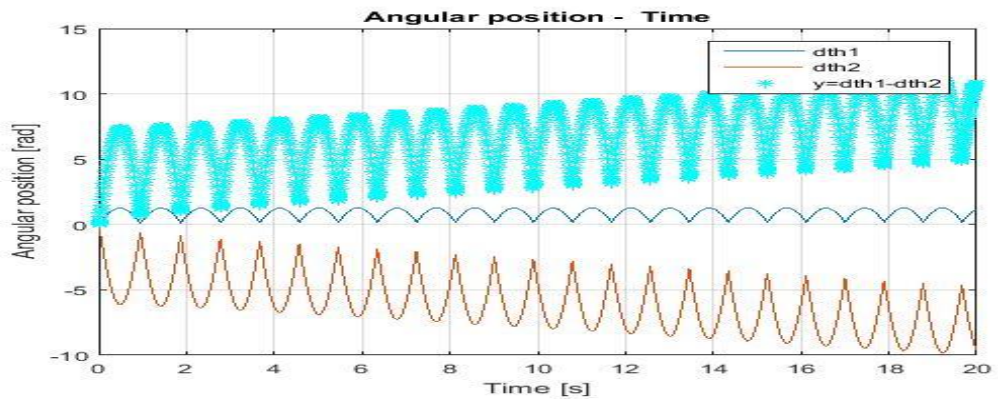


Fig. 7: Different between $d\theta_1$ and $d\theta_2$

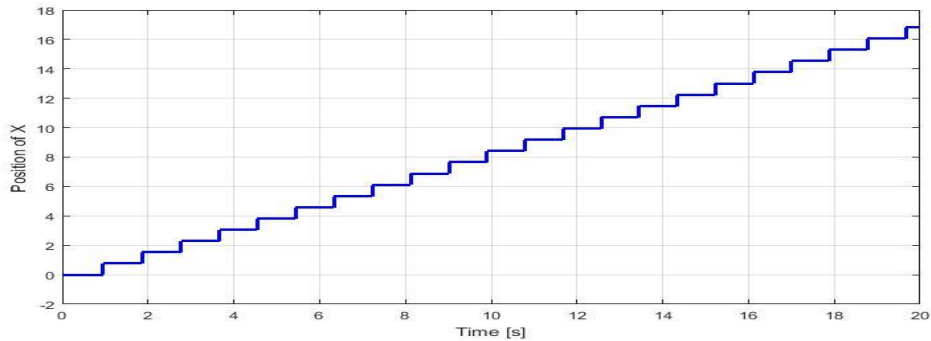


Fig. 8: Position of x

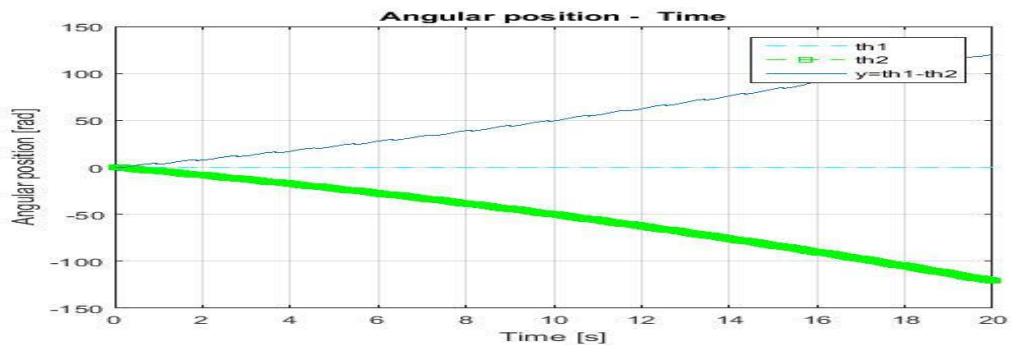


Fig. 9: Angular position of dh1 and th1

6. Conclusion

This examination portrays the underactuated rimless wheel with middle which driven on level ground and likeness with biped strolling automated mechanism. We built up the scientific model of 4-DOF URW with middle which can be driven on level ground. We connected here condition of motion. During the numerical recreation, we attempted ordinarily for an appropriate control framework and accomplish a steady step age.

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Author's Biography



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